

CHAPTER 4

PLANE GRIDCONTENTS

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4.1 Introduction

The material presented in Chapters I and II of this manual are a necessary prerequisite for a reasonable understanding of the material presented in this chapter.

STRUDL treats a plane grid structure as a system of members lying in a plane, rigidly connected at their ends. The individual members must have one of their principal axes in the plane of the grid. The centroidal axis of each member will be the local X-axis. Each member is assumed to have the shear center axis at the longitudinal axis (local X-axis). Bending and torsion occur independently of one another if the shear center is taken as the longitudinal axis. For members symmetrical about both principal axes the shear center is actually located at the centroid of the member.

All forces applied to the grid must be normal to the plane of the structure and all couples must have their moment vectors in the plane of the grid. The significant member displacements are the rotations about the two member axes in the plane of the structure. Shear deformations may also be considered in the analysis of members which have appreciable depth relative to their lengths. A brief review of shearing deformations is presented in Chapter I. Axial deformations are not considered in the analysis, thus in-plane membrane action is not considered.

STRUDL considers only uniform torsion. The effects of restrained torsion or warping are not considered in the analysis. For concrete bridge structures made up of relatively thick members the effects of warping are negligible and STRUDL will provide accurate results. For open, thin-walled cross sections such as ordinary steel rolled beams, the effect of restrained torsion or warping may be important, in which case the STRUDL analysis would not be applicable.

A plane grid structure may be placed on any one of the three global coordinate planes. However, the user can simplify the formulation and visualization of plane grid structures by placing them in the global XZ plane. In this plane the positive local Y axis of the individual members is in the same direction as the positive global Y axis for Beta = 0. Thus the required member properties, for Beta = 0, will be IX, the torsional rigidity, and IZ, the moment of inertia.

The STRUDL grid analysis can be used to approximate the behavior of bridge decks by using an equivalent grid idealization, i.e., by replacing the bridge deck by a framework of slender beam elements. The longitudinal members being a combination of the composite or non-composite girder and a strip of deck slab interconnected by transverse members to form a grid. The torsional rigidity of the system can be approximated by inducing torsional rigidities into the individual members.

Using the new finite element capability available in STRUDL II, a bridge deck can be analyzed as an idealized continuum using equivalent plate elements interconnected by beam elements. The finite element capability will be discussed in Chapter VII.

4.2 Plane Grid Problem (with SAVE command)

To illustrate the analysis of a plane grid structure and some additional STRUDL commands, consider the grid structure shown in Figure 4.2a. Subjected to the loading conditions shown in Figure 4.2d.

The STRUDL SAVE and RESTORE capabilities are illustrated in this problem.

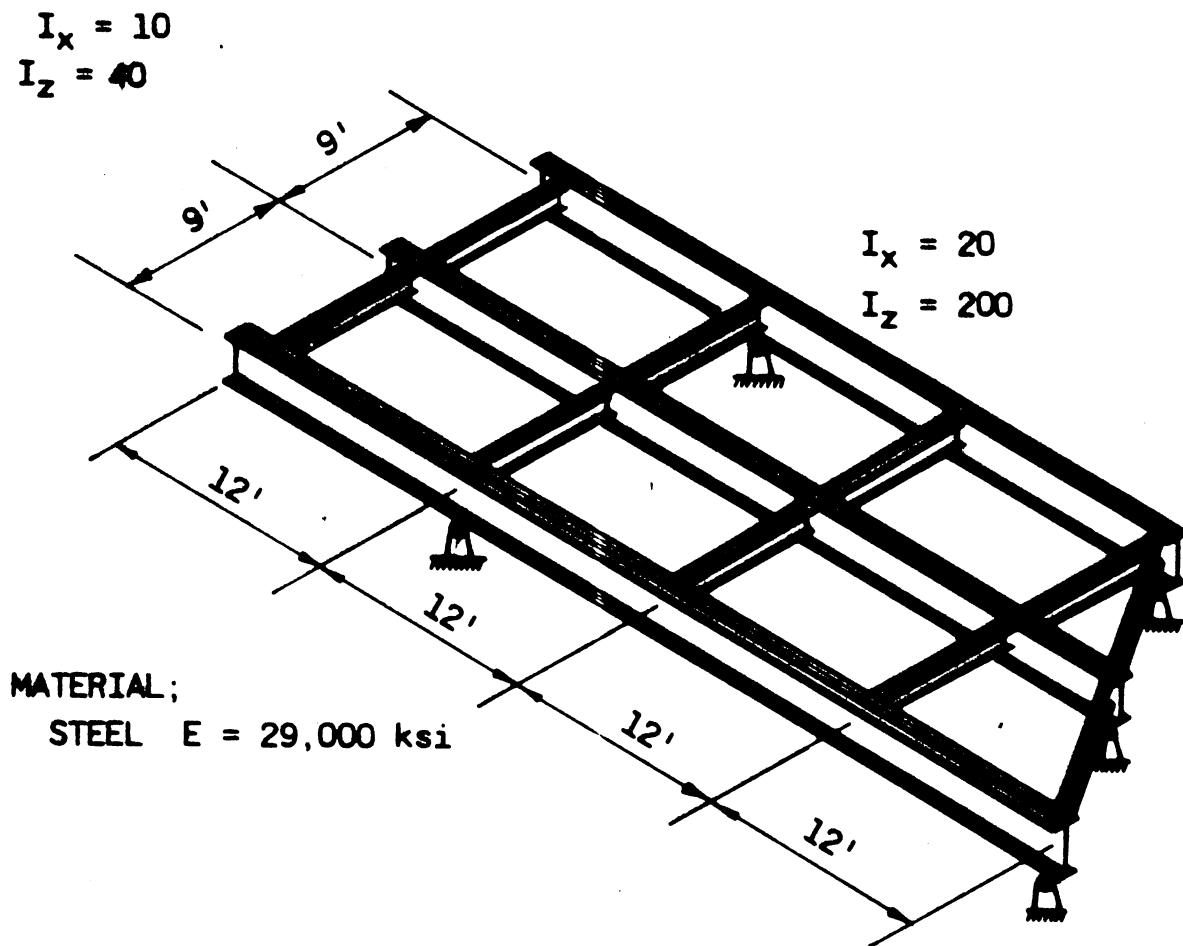


Fig. 4.2 a

The location of the global axes and the joint member numbering scheme is shown in Figure 4.2b.

The plane grid is located in the XZ plane.

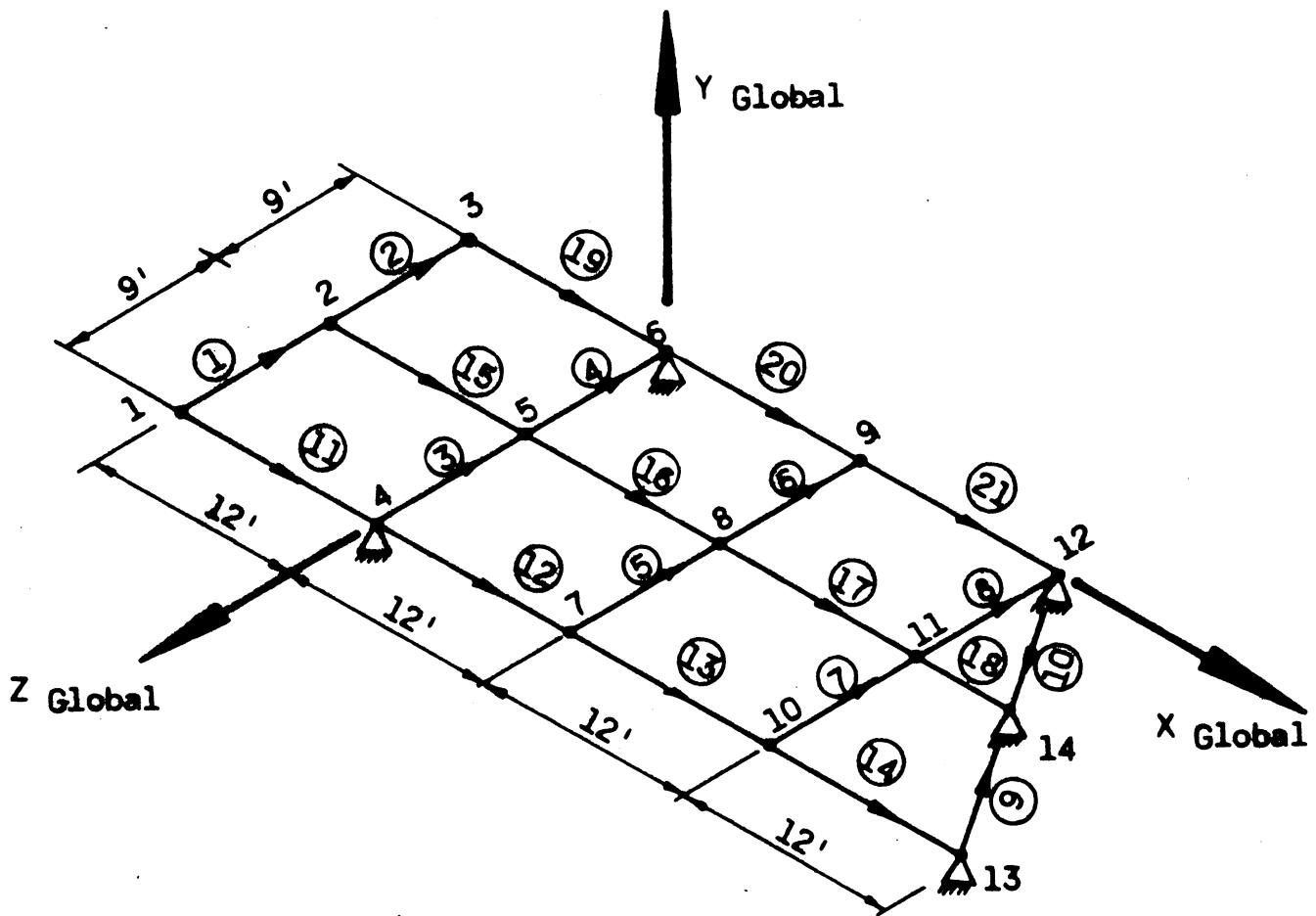


Fig. 4.2b

The basic structure geometry is described in lines 10 thru 410 of the coding below. Note that joints 1 to 3 are located with negative X coordinates. Joint coordinates are located relative to any right-handed orthogonal axes system and may have either a positive or negative value.

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COMPUTER SYSTEMS

ICES

		ADDRESS	BATCH
b	b	DIST. GROUP	
3 JAN 27			
14 55 04 07 55 00 70 71 72			

SUBSYSTEM NAME	0	1	SOURCE	CHARGE	EXPENDITURE	SPECIAL DESIGNATION	b	SEQUENCE
	b	b	DIST. UNIT	DIST. UNIT	AUTHORIZATION	WHERE APPLICABLE	b	
STRUDL 'PROB. 4.2' 'PLANE GRID'	\$							1
1 2 4 6 8 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72							73 74 75 76	
TYPE PLANE GRID XZ								20
UNITS FEET								30
JOINT COORDINATES								40
1 -12. Z 18.								50
2 -12. Z 9.								60
3 -12.								70
4 Z 18. SUPPORT								80
5 Z 9.								90
6 SUPPORT								100
7 12. Z 18.								110
8 12. Z 9.								120
9 12.								130
10 24. Z 18.								140
11 24. Z 9.								150
12 24. SUPPORT								160
13 36. Z 18. SUPPORT								170
14 30. Z 9. SUPPORT								180
JOINTS 4 6 12 13 14 RELEASE MOMENTS X Z								190
MEMBER INCIDENCES								200
1 1 2								210
2 2 3								220
3 4 5								230
4 5 6								240
5 7 8								250
6 8 9								260
7 10 11								270
8 11 12								280
9 13 14								290
10 12 14								300
11 1 4								310
12 4 7								320
13 7 10								330
14 10 13								340
15 2 5								350
16 5 8								360
17 8 11								370
18 11 14								380
19 3 6								390
20 6 9								400
21 9 12								410
MEMBERS 3 THRU 8 RELEASE START MOMENT Z END MOMENT Z								420

Line 0420 illustrates the use of the individual form of the MEMBER RELEASE statement. The MEMBER RELEASE statement is used to define the start and end releases of any member. (JOINT RELEASES on the other hand apply only to support joints.)

In a PLANE GRID structure we must consider the effect of our connections upon the end restraint of the members. For the beam connection in Figure 4.2c the support angles affect the end fixity of the beam. The possible components for release from the full fixity are: Force Y, Moment X and Moment Z.

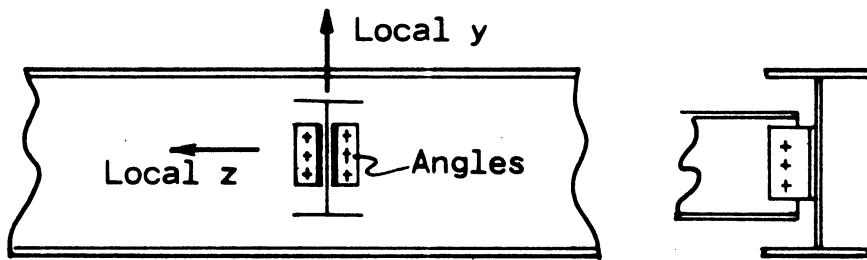


Fig. 4.2c

Members 1-8 End Connection (Problems 4.2 & 4.3)

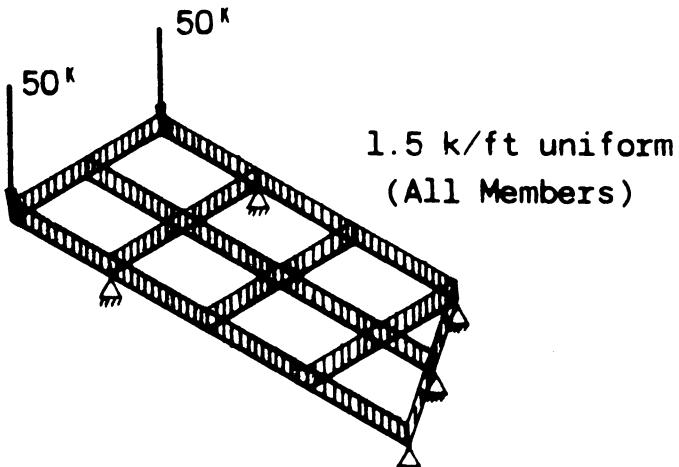
If we consider the angles to be so small that they would not offer any torsional restraint (Moment X) or bending restraint (Moment Z) the appropriate releases would be Moment X and Moment Z. Moment X (Torsion) should not be released at both ends of a member because it would be free to spin on its X-axis yielding an unstable member.

For this problem we will assume the angles to be capable of transmitting shear and torsion. The release to be specified will be Moment Z at both ends of members 3 to 8 as coded on line 420.

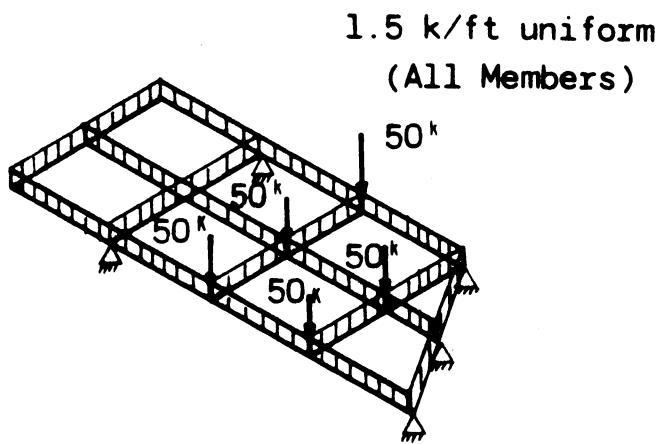
The commands shown below on lines 430 to 470 describe the elastic properties and the member properties of the structure.

UNITS	KIPS	INCHES												430
CONSTANTS	E	29000.	ALL											440
MEMBER PROPERTIES	PRISMATIC													450
1.	THRU	10.	I	X.	10..	1Z	40.0							460
11.	THRU	21	I	X.	20..	1Z	200.0							470

UNITS FEET	480
LOADING 'ONE'	490
JOINTS 1, 3 LOAD FORCE Y -50	500
MEMBERS 1 THRU 21 LOAD FORCE Y UNIFORM -1.5	510
LOADING 'TWO'	511
JOINTS 7 TO 11 LOAD FORCE Y -50	512
MEMBERS 1 TO 21 LOAD FORCE Y UNIF. -1.5	513



LOADING 'ONE'



LOADING 'TWO'

Fig. 4.2d

The two loading conditions shown in Figure 4.2d are coded on lines 490 thru 513. The structure and the two loading conditions are now completely described.

The commands appearing on lines 520 to 570 instruct the computer to print the problem description as interpreted by STRUDL, perform an analysis and printout the resulting forces, reactions and displacements.

LOADING LIST ALL	520
UNITS INCHES	530
PRINT DATA	540
SLEFFNESS ANALYSIS	550
UNITS FEET KIPS	560
LST. FORCES REACTIONS	570
SAVE 'PROB 4.2'	600

The last command, SAVE 'PROB. 4.3', given on line 600 instructs the computer to save the problem on secondary storage. The problem will be saved with the current status of the problem for a period of time requested in the JOB CONTROL LANGUAGE. The user should contact a STRUDL coordinator prior to submitting a problem to be saved for assistance in this area. In Problem 4.3 this problem is restored, modified, reanalyzed and saved again.

STRUOL 'PROB 4.2' 'PLANE GRID' \$ 14N 27 0010

* ICES STRUOL II VERSION 1 MOD 1 *
* THE STRUCTURAL DESIGN LANGUAGE *
* MASSACHUSETTS INSTITUTE OF TECHNOLOGY *
* STATE OF CALIFORNIA *
* BRIDGE DEPARTMENT DIVISION OF HWYS. *
* SPECIAL STUDIES SECTION PH. 445-6519 *
* NOVEMBER 1969 INSTALLED APRIL 1970 *
* 21:45:01 8/31/70 *
* *****

TYPE PLANE GRID XZ	\$ 14N 27	0020
UNITS FEET	\$ 14N 27	0030
JOINT COORDINATES	\$ 14N 27	0040
1 -12. Z 18.	\$ 14N 27	0050
2 -12. Z 9.	\$ 14N 27	0060
3 -12.	\$ 14N 27	0070
4 Z 18. SUPPORT	\$ 14N 27	0080
5 Z 9.	\$ 14N 27	0090
6 SUPPORT	\$ 14N 27	0100
7- 12. Z 18.	\$ 14N 27	0110
8 12. Z 9.	\$ 14N 27	0120
9 12.	\$ 14N 27	0130
10 24. Z 18.	\$ 14N 27	0140
11 24. Z 9.	\$ 14N 27	0150
12 24. SUPPORT	\$ 14N 27	0160
13 36. Z 18. SUPPORT	\$ 14N 27	0170
14 30. Z 9. SUPPORT	\$ 14N 27	0180
JOINTS 4 6 12 13 14 RELEASE MOMENTS X Z	\$ 14N 27	0190
MEMBER INCIDENCES	\$ 14N 27	0200
1 1 2	\$ 14N 27	0210
2 2 3	\$ 14N 27	0220
3 4 5	\$ 14N 27	0230
4 5 6	\$ 14N 27	0240
5 7 8	\$ 14N 27	0250

6 8 9	\$ 14N 27	0260
7 10 11	\$ 14N 27	0270
8 11 12	\$ 14N 27	0280
9 13 14	\$ 14N 27	0290
10 12 14	\$ 14N 27	0300
11 1 4	\$ 14N 27	0310
12 4 7	\$ 14N 27	0320
13 7 10	\$ 14N 27	0330
14 10 13	\$ 14N 27	0340
15 2 5	\$ 14N 27	0350
16 5 8	\$ 14N 27	0360
17 8 11	\$ 14N 27	0370
18 11 14	\$ 14N 27	0380
19 3 6	\$ 14N 27	0390
20 6 9	\$ 14N 27	0400
21 9 12	\$ 14N 27	0410
MEMBERS 3 THRU 8 RELEASE START MOMENT Z END MOMENT Z	\$ 14N 27	0420
UNITS KIPS INCHES	\$ 14N 27	0430
CONSTANTS E 29000. ALL	\$ 14N 27	0440
MEMBER PROPERTIES PRISMATIC	\$ 14N 27	0450
1 THRU 10 IX 10. IZ 40.0	\$ 14N 27	0460
11 THRU 21 IX 20. IZ 200.0	\$ 14N 27	0470
UNITS FFET	\$ 14N 27	0480
LOADING 'ONE'	\$ 14N 27	0490
JOINTS 1 3 LOAD FORCE Y -50.	\$ 14N 27	0500
MEMBERS 1 THRU 21 LOAD FORCE Y UNIFORM -1.5	\$ 14N 27	0510
LOADING 'TWO'	\$ 14N 27	0511
JOINTS 7 TO 11 LOAD FORCE Y -50.	\$ 14N 27	0512
MEMBERS 1 TO 21 LOAD FORCE Y UNIF -1.5	\$ 14N 27	0513
LOADING LIST ALL	\$ 14N 27	0520
UNITS INCHES	\$ 14N 27	0530
PRINT DATA	\$ 14N 27	0540

* PROBLEM DATA FROM INTERNAL STORAGE *

JOB ID - PROR 4.2 JOB TITLE - PLANE GRID

ACTIVE UNITS - LENGTH WEIGHT ANGLE TEMPERATURE TIME
INCH KIP RAD DEGF SEC

***** STRUCTURAL DATA *****

ACTIVE STRUCTURE TYPE - PLANE GRID

ACTIVE COORDINATE AXES X Z

JOINT COORDINATES-----/ STATUS---/
JOINT X Y Z CONDITION

1	-144.000	0.0	216.000	ACTIVE
2	-144.000	0.0	108.000	ACTIVE
3	-144.000	0.0	0.0	ACTIVE
4	0.0	0.0	216.000	SUPPORT ACTIVE
5	0.0	0.0	108.000	ACTIVE
6	0.0	0.0	0.0	SUPPORT ACTIVE
7	144.000	0.0	216.000	ACTIVE
8	144.000	0.0	108.000	ACTIVE
9	144.000	0.0	0.0	ACTIVE
10	288.000	0.0	216.000	ACTIVE
11	288.000	0.0	108.000	ACTIVE
12	288.000	0.0	0.0	SUPPORT ACTIVE
13	432.000	0.0	216.000	SUPPORT ACTIVE
14	360.000	0.0	108.000	SUPPORT ACTIVE

JOINT RELEASES-----/ ELASTIC SUPPORT RELEASES-----/
JOINT FORCE MOMENT THETA 1 THETA 2 THETA 3 KFX KFY KFZ KMX KMY KNZ
4 X Z 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
6 X Z 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
12 X Z 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
13 X Z 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
14 X Z 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0

MEMBER INCIDENCES-----/ LENGTH-----/ RELEASES-----/ STATUS--/
MEMBER START END LOCAL COORD. START END
FORCE MOMENT FORCE MOMENT

1	1	2	108.000				ACTIVE
2	2	3	108.000				ACTIVE
3	4	5	108.000	Z	Z	Z	ACTIVE
4	5	6	108.000	Z	Z	Z	ACTIVE
5	7	8	108.000	Z	Z	Z	ACTIVE
6	8	9	108.000	Z	Z	Z	ACTIVE
7	10	11	108.000	Z	Z	Z	ACTIVE
8	11	12	108.000	Z	Z	Z	ACTIVE
9	13	14	129.000				ACTIVE
10	12	14	129.000				ACTIVE
11	1	4	144.000				ACTIVE
12	4	7	144.000				ACTIVE
13	7	10	144.000				ACTIVE
14	10	13	144.000				ACTIVE
15	2	5	144.000				ACTIVE
16	5	8	144.000				ACTIVE
17	8	11	144.000				ACTIVE
18	11	14	72.000				ACTIVE
19	3	6	144.000				ACTIVE
20	6	9	144.000				ACTIVE
21	9	12	144.000				ACTIVE

MEMBER PROPERTIES-----/		SEG-L	COMP	AX/YD	AY/ZD	AZ/YC	TX/ZC	TY/EY	TZ/EZ	SY	SZ
MEMBER/SEG TYPE											
.1	PRISMATIC			0.0	0.0	0.0	10,000	0.0	40,000	0.0	0.0
				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
.2	PRISMATIC			0.0	0.0	0.0	10,000	0.0	40,000	0.0	0.0
				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
.3	PRISMATIC			0.0	0.0	0.0	10,000	0.0	40,000	0.0	0.0
				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
.4	PRISMATIC			0.0	0.0	0.0	10,000	0.0	40,000	0.0	0.0
				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
.5	PRISMATIC			0.0	0.0	0.0	10,000	0.0	40,000	0.0	0.0
				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
.6	PRISMATIC			0.0	0.0	0.0	10,000	0.0	40,000	0.0	0.0
				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
.7	PRISMATIC			0.0	0.0	0.0	10,000	0.0	40,000	0.0	0.0
				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
.8	PRISMATIC			0.0	0.0	0.0	10,000	0.0	40,000	0.0	0.0
				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
.9	PRISMATIC			0.0	0.0	0.0	10,000	0.0	40,000	0.0	0.0
				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
.10	PRISMATIC			0.0	0.0	0.0	10,000	0.0	40,000	0.0	0.0
				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
.11	PRISMATIC			0.0	0.0	0.0	20,000	0.0	200,000	0.0	0.0
				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
.12	PRISMATIC			0.0	0.0	0.0	20,000	0.0	200,000	0.0	0.0
				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
.13	PRISMATIC			0.0	0.0	0.0	20,000	0.0	200,000	0.0	0.0
				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
.14	PRISMATIC			0.0	0.0	0.0	20,000	0.0	200,000	0.0	0.0
				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
.15	PRISMATIC			0.0	0.0	0.0	20,000	0.0	200,000	0.0	0.0
				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
.16	PRISMATIC			0.0	0.0	0.0	20,000	0.0	200,000	0.0	0.0
				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
.17	PRISMATIC			0.0	0.0	0.0	20,000	0.0	200,000	0.0	0.0
				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
.18	PRISMATIC			0.0	0.0	0.0	20,000	0.0	200,000	0.0	0.0
				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
.19	PRISMATIC			0.0	0.0	0.0	20,000	0.0	200,000	0.0	0.0
				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
.20	PRISMATIC			0.0	0.0	0.0	20,000	0.0	200,000	0.0	0.0
				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
.21	PRISMATIC			0.0	0.0	0.0	20,000	0.0	200,000	0.0	0.0
				0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

MEMBER CONSTANTS-----/			
CONSTANT	STANDARD	VALUE	DOMAIN
E	28999.996094	ALL	
G	0.0	ALL	
DENSITY	0.001000	ALL	
CTE	1.000000	ALL	
BETA	0.0	ALL	
POISSON	0.0	ALL	

STIFFNESS ANALYSIS	\$ 14N 27	0550
UNITS FEET KIPS	\$ 14N 27	0560
LIST FORCES REACTIONS DISPLACEMENTS	\$ 14N 27	0570

SAVE 'PROB 4.2'

\$ 14N 27 0600

FINISH

0000

GOOD-BYE

Results

The interpretation of output results for several members of the plane grid structure analyzed are illustrated using the free body diagrams on the following pages. The torsional couples and bending moments are drawn with double headed arrows in the direction of the local coordinate axes, the sense being determined by the sign of the reported force. The actual moments and torques act in planes normal to the arrows, their direction being determined by the right hand screw rule. Following is a statement of the rule:

Point the right hand thumb in the direction of the moment or torque vector. Fingers now point in the direction of the actual moment or torque.

To illustrate the application of the right hand rule, consider the free body diagram of member 11 shown in Figure 4.2e below.

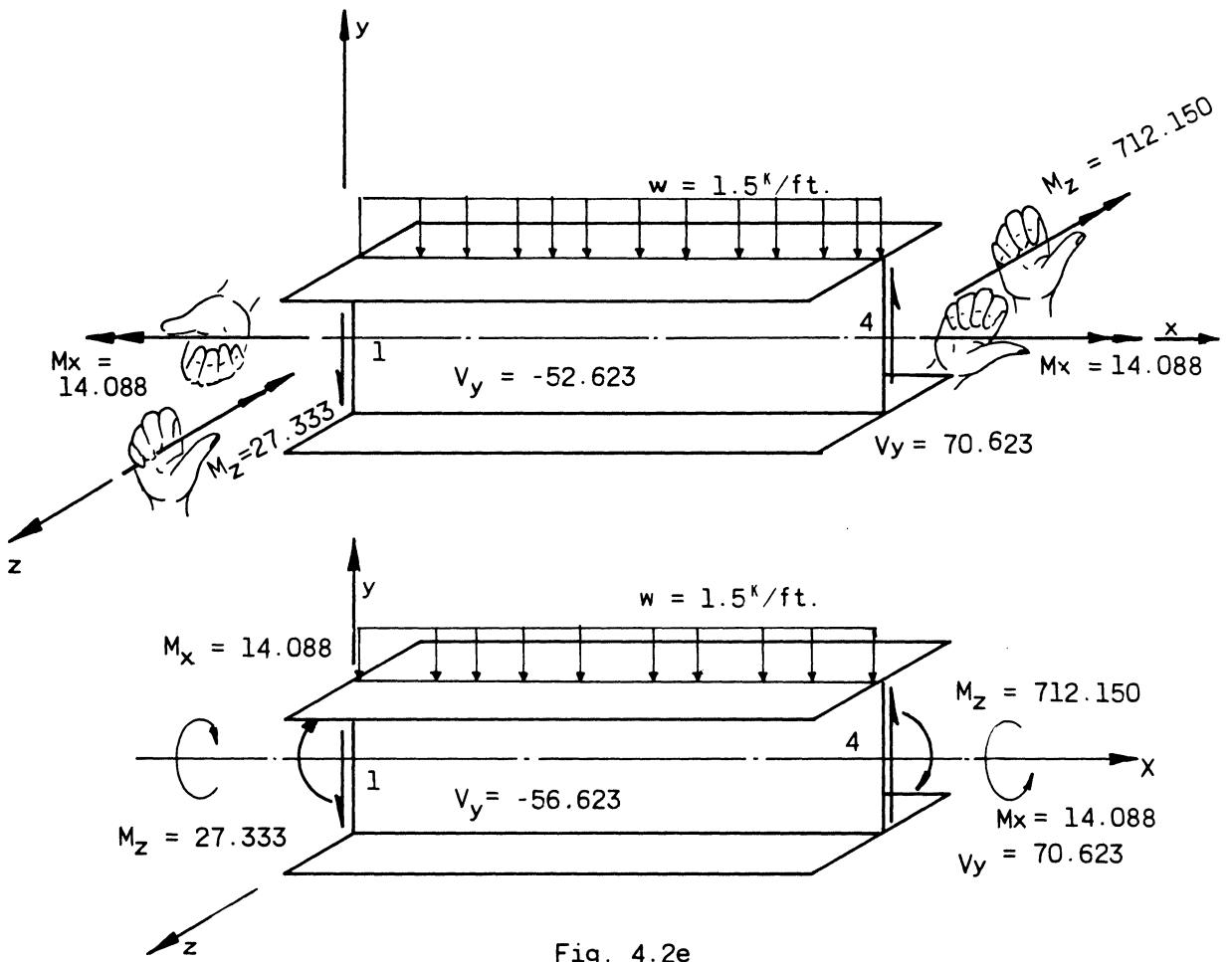


Fig. 4.2e

LOADING - TWO

MEMBER FORCES

MEMBER	JOINT	FORCE	SHEAR Y	TORSIONAL	BENDING Z
11	1		-52.6235809	-14.0877104	-27.3325195
11	4		70.6235504	14.0877104	-712.1503906

The output results for the members end forces of member 11 are shown above. The double headed torque (M_x) and moment (M_z) vectors are shown in the upper free body diagram, their direction being determined directly from the output results. The right hand rule is applied to the vectors to determine how the torques and moments act on the ends of the member as shown in the lower free body diagram.

Shown in Figure 4.2f below is a free body diagram of joint 4, followed by the output results for the members meeting at joint 4 and the resulting joint forces at joint 4 for LOADING TWO.

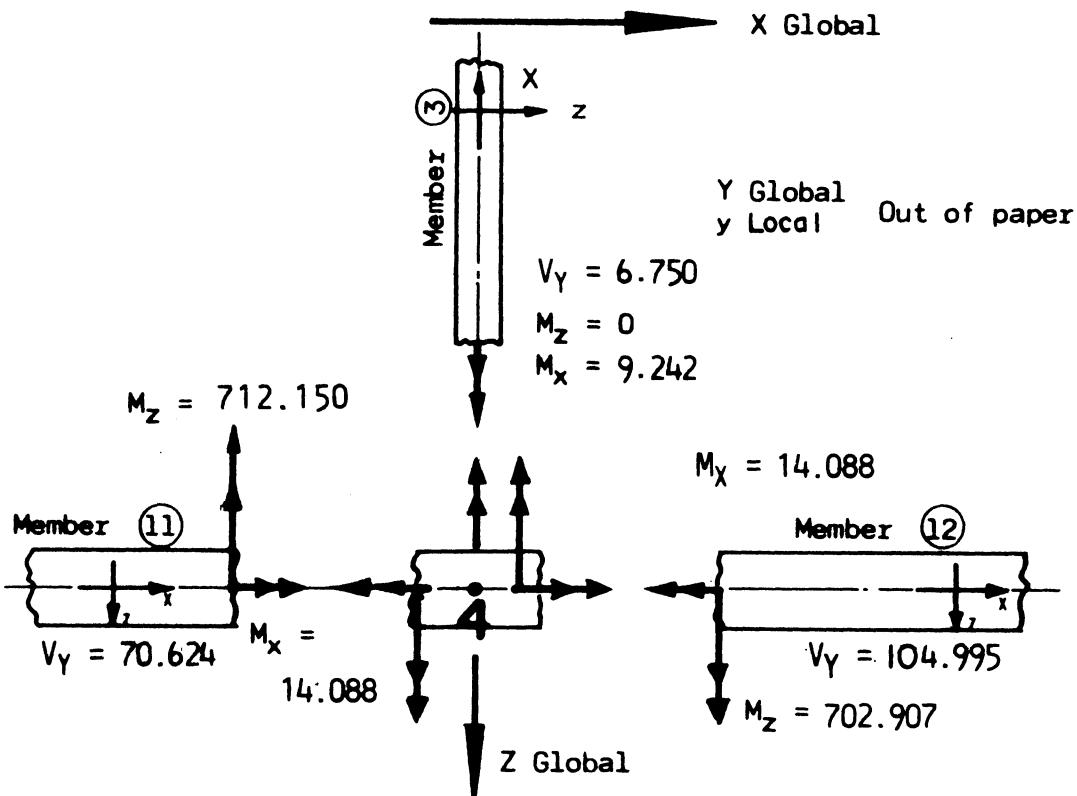


Fig. 4.2f

LOADING - TWO

MEMBER FORCES

MEMBER	JOINT	FORCE -----	SHEAR Y	TORSIONAL	BENDING Z
3	4		6.7499990	-9.2423000	0.0
3	5		6.7499994	9.2423000	0.0
11	1		-52.6235809	-14.08771C4	-27.3325195
11	4		70.6235504	14.08771C4	-712.1503906
12	4		104.9951172	-14.08771C4	702.9079590
12	7		-86.9951172	14.08771C4	449.0334473

RESULTANT JOINT LOADS - SUPPORTS

JOINT	FORCE ----- /	Y FORCE	X MOMENT	Z MOMENT
4		182.3687285	0.0	0.0000000

The vectors of the moments and torques acting on the ends of the members are directed as indicated by the output results in the local coordinate system for each of the members. Equal and opposite torques and moments acting on joint 4 are also shown in the diagram. These forces are in the global coordinate system. Resolution of the member end forces applied to the joint should be equal and opposite to the forces reported for the RESULTANT JOINT LOADS - SUPPORTS for joint 4. These forces are resolved in the calculations below, note that the results are equal and opposite to the results reported at joint 4 and the joint is in equilibrium.

$$M_x = -14.0877 + 14.0877 = 0.0000 \text{ KIP FT.}$$

$$M_z = 712.1504 - 9.2423 - 702.9079 = 0.0002 \text{ KIP FT.}$$

$$V_y = -70.6236 - 6.7500 - 104.9951 = 182.3687 \text{ KIPS}$$

To further illustrate this technique consider a more general case with non-orthogonal members meeting at a joint such as at joint 13 shown in Figure 4.2g. The output results for the members meeting at the joint and the joint follow.

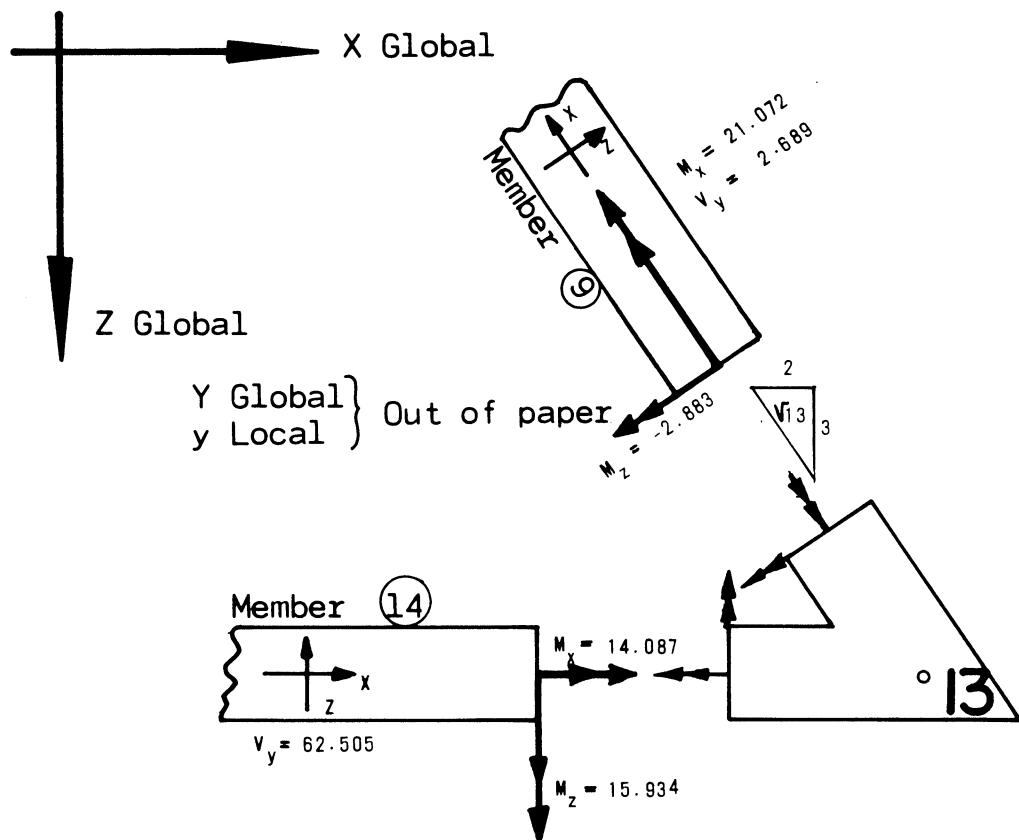


Fig. 4.2g

LOADING - TWO

MEMBER FORCES

MEMBER	JOINT	FORCE	SHEAR Y	TORSIONAL	BENDING Z
9	13		2.6890841	21.0722198	-2.8831692
9	14		13.5358896	-21.0722198	-55.7799377
14	10		-44.5047913	-14.0877104	-657.9914551
14	13		62.5047913	14.0877104	15.9338560

RESULTANT JOINT LOADS - SUPPORTS

JOINT	FORCE ----- /		
	Y FORCE	X MOMENT	Z MOMENT
13	65.1939792	0.0000023	-0.0000027

The vectors of the moments and the torque acting on the members are directed as indicated by the output results. Equal and opposite forces act on the joint as shown on the free body diagram. These forces now acting in the global coordinate system must be resolved into the direction of the global coordinate axes. The forces are resolved in the following calculations and agree with those reported in the output results for the RESULTANT JOINT LOADS - SUPPORTS.

$$\begin{aligned}\Sigma M_x &= -14.0877 + \frac{3}{\sqrt{13}} (2.8832) + \frac{2}{\sqrt{13}} (21.0722) \\ &= -14.0877 + 2.3990 + 11.6888 = +.0001 \text{ KIP FT.}\end{aligned}$$

$$\begin{aligned}\Sigma M_z &= -15.9338 - \frac{2}{\sqrt{13}} (2.8832) + \frac{3}{\sqrt{13}} (21.0722) \\ &= -15.9338 - 1.5993 + 17.5331 = .0000 \text{ KIP FT.}\end{aligned}$$

$$\Sigma V_y = -62.5048 - 2.6890 = -65.1938 \text{ KIPS}$$

4.3 Revised Plane Grid Problem (with RESTORE command)

The plane grid structure shown in Figure 4.2a will now be revised by removing the support as shown in Figure 4.3a below:

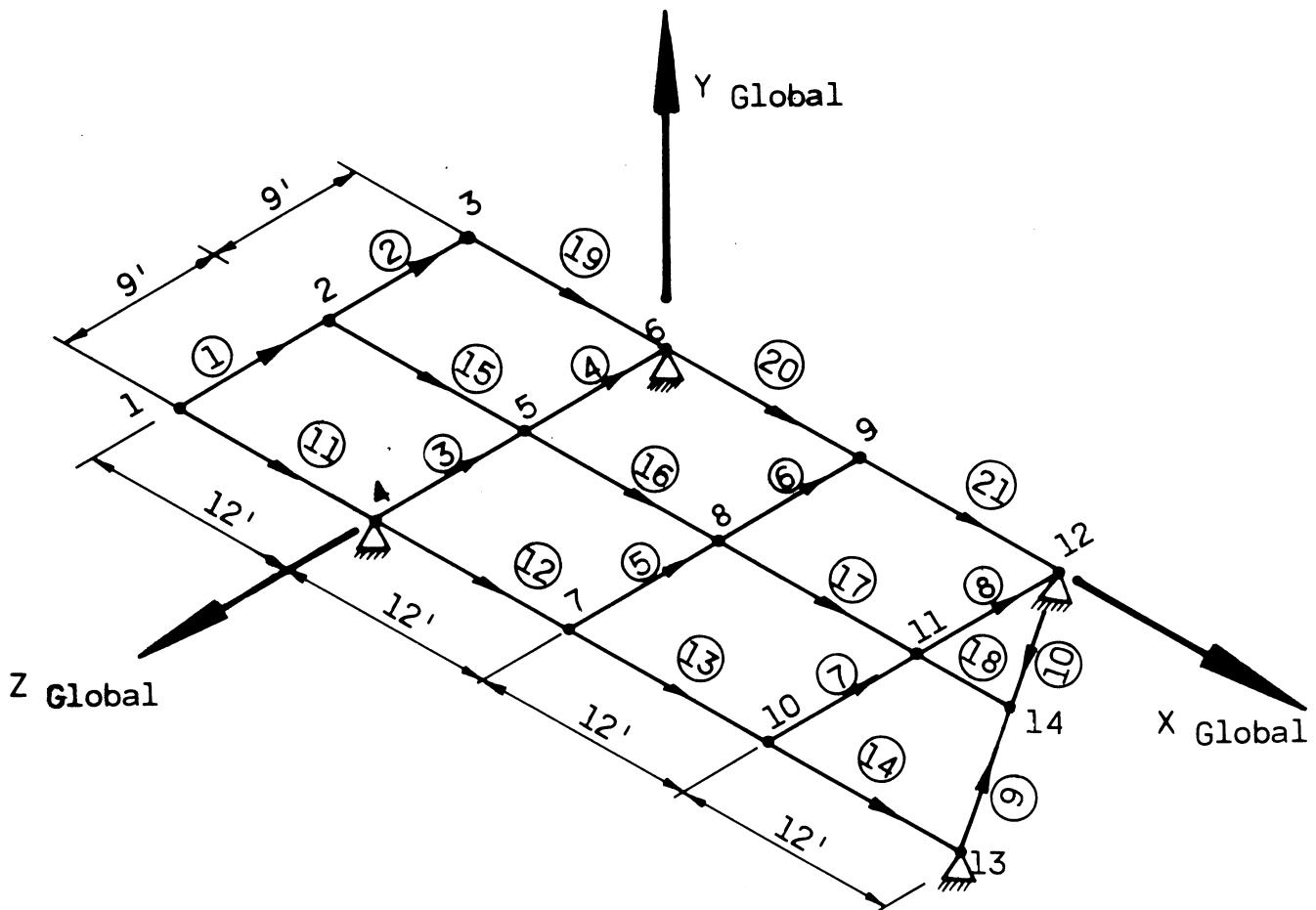


Fig. 4.3a

The revised structure will be reanalyzed for the loading conditions shown in Figure 4.2d. The command STRUDL RESTORE 'PROB. 4.2' given on line 0010 restores the problem with the same status that it had when it was saved in the previous problem. The commands shown on lines 0020 thru 0060 are given to revise the structure. Following these are commands requesting print out of the STRUDL interpretation of the revised structure. The structure is then reanalyzed and saved for a subsequent analysis. The STRUDL output for the revised structure is on the following pages.

COMPUTER SYSTEMS

ICES

NUMBER 60
DATE 1/14/24
64 65 66 67 68 69 70 71 72

SUBSYSTEM NAME	1 b	SOURCE	CHARGE	EXPENDITURE	SPECIAL DESIGNATION WHEN APPLICABLE	b	SEQUENCE
	1 b	DIST. UNIT	DIST. UNIT	AUTHORIZATION		b	6 6 6 1
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63							73747970
STRUDL RESTORE 'PROB 4.2'							10
DELETIONS							20
JOINT 14 RELEASES MOMENT X Z							30
CHANGES							40
JOINT 14 COORDINATES FREE							50
CHANGE ID 'PROB 4.3' 'PROB 4.2' WITH JOINT 14 SUPPORT REMOVED							60
UNITS INCHES							70
PRINT JOINT COORDINATES							80
PRINT JOINT RELEASES							90
STIFFNESS ANALYSIS							100
UNITS FEET KIPS							110
LIST FORCES REACTIONS DISPLACEMENTS							120

```
*****
*      ICES STRU DL II      VERSION 1 MOD 1
*      THE STRUCTURAL DESIGN LANGUAGE
*      MASSACHUSETTS INSTITUTE OF TECHNOLOGY
*      STATE OF CALIFORNIA
*      BRIDGE DEPARTMENT DIVISION OF HWYS.
*      SPECIAL STUDIES SECTION PH. 445-6519
*      NOVEMBER 1969 INSTALLED APRIL 1970
*      20:12:54      9/01/70
*
*****
```

DEFLECTIONS	\$ 14N 28	0020
JOINT 14 RELEASES MOMENT X 7	\$ 14N 28	0030
CHANGES	\$ 14N 28	0040
JOINT 14 COORDINATES FREE	\$ 14N 28	0050
CHANGE ID 'PROB 4.3' 'PROB 4.2 WITH JOINT 14 SUPPORT REMOVED	\$ 14N 28	0060
UNITS INCHES	\$ 14N 28	0070
PRINT JOINT COORDINATES	\$ 14N 28	0080

```
*****
* PROBLEM DATA FROM INTERNAL STORAGE *
*****
```

JOB ID - PROB 4.3 JOB TITLE -

ACTIVE UNITS - LENGTH		WEIGHT	ANGLE	TEMPERATURE	TIME
JOINT COORDINATES - INCH		-KIP-	-RAD-	/ DEGF	SFC
JOINT	X	Y	Z	CONDITION	
1	-144.000	0.0	216.000		
2	-144.000	0.0	108.000		
3	-144.000	0.0	0.0		
4	0.0	0.0	216.000	SUPPORT	
5	0.0	0.0	108.000		
6	0.0	0.0	0.0	SUPPORT	
7	144.000	0.0	216.000		
8	144.000	0.0	108.000		
9	144.000	0.0	0.0		
10	288.000	0.0	216.000		
11	288.000	0.0	108.000		
12	288.000	0.0	0.0	SUPPORT	
13	432.000	0.0	216.000	SUPPORT	
14	360.000	0.0	108.000		

JOINT RELEASES-----/ELASTIC SUPPORT RELEASES-----/											
JOINT	FORCE	MOMENT	THETA 1	THETA 2	THETA 3	KFX	KFY	KFZ	KX	KY	KZ
4	X	Z	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
6	X	Z	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
12	X	Z	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
13	X	Z	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

```
*****
* END OF DATA FROM INTERNAL STORAGE *
*****
```

PRINT JOINT RELEASES

\$ 14N 28 0090

* PROBLEM DATA FROM INTERNAL STORAGE *

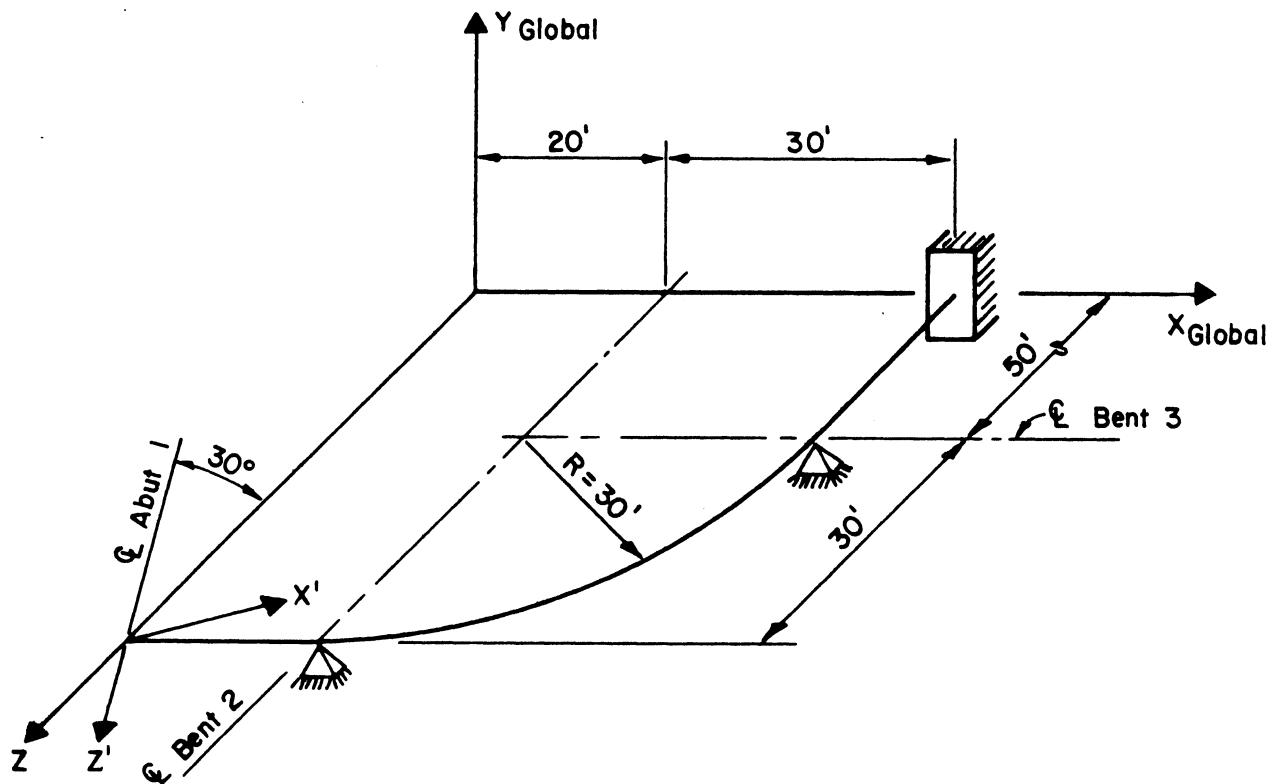
JOB ID - PPAR 4.3 JOB TITLE -

I 5 ~

ACTIVE UNITS - LENGTH		WEIGHT	ANGLE	TEMPERATURE	TIME	JOINT RELEASES-----/					
JOINT	FORCE	MOMENT	THETA 1	THETA 2	THETA 3	KFX	KFY	KFZ	KMX	KMY	KMZ
4	X	Z	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
6	X	Z	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
12	X	Z	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
13	X	Z	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

* END OF DATA FROM INTERNAL STORAGE *

4.4 EXAMPLE PLANE GRID PROBLEM



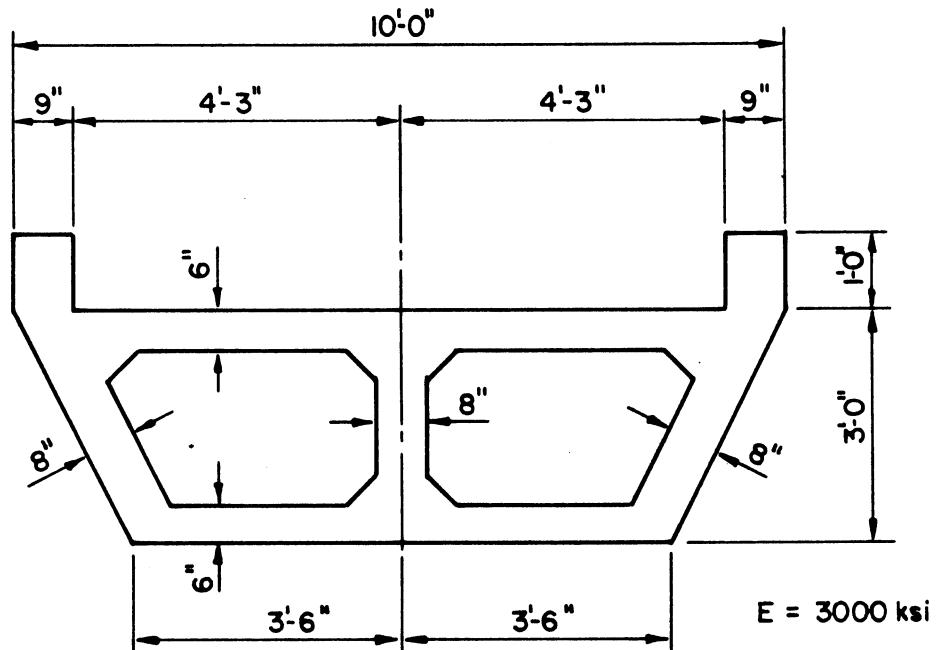
Using STRUDL determine the following for the grid structure shown in the sketch above:

1. The member forces at the 1/5 points for all three spans due to the imposed dead load and overturning force. Use 2200 pounds per ft. for the dead load. The overturning force is 200 pounds per foot and is applied at the right edge of the soffit.
2. The live load moment envelope, local moment Z, for the curved span. Use the 1/5 points also for the moment envelope. The intensity of the live loading is 85 pounds per square foot.

3. The torsional constant I_X , for the two celled box section using the method of simultaneous equations or the method of successive corrections as outlined in Appendix C of the Bridge STRUDL manual. Compare the torsional constant computed using one of these two methods with the torsional constant computed neglecting the interior web. The torsional constants for standard closed sections are also given in this appendix on page C-6.

Include the curb sections in calculating the torsional stiffness.

Note the skew angle at Abutment 1. The support conditions at the abutment are such that the structure is restrained from rotating about the X' axis and free to rotate about the Z' axis.



TYPICAL SECTION

The ICES/STRU DL coding for this problem is as follows:

STRU DL *PROB 4.4* *EXAMPLE PLANE GRID PROBLEM, POC*	\$	14T 60	0010
\$	\$	14T 60	0020
TYPE PLANE GRID XZ	\$	14T 60	0030
UNITS FEET KIPS DEGREES	\$	14T 60	0040
JOINT COORDINATES	\$	14T 60	0100
1 0. 0. 80. SUPPORT	\$	14T 60	0110
2 20. 0. 80. SUPPORT	\$	14T 60	0120
3 29.271 0. 78.532	\$	14T 60	0130
4 37.634 0. 74.271	\$	14T 60	0140
5 44.271 0. 67.634	\$	14T 60	0150
6 48.532 0. 59.271	\$	14T 60	0160
7 50.000 0. 50.000 SUPPORT	\$	14T 60	0170
8 50.000 0. 0. SUPPORT	\$	14T 60	0180
MEMBER INCIDENCES	\$	14T 60	0200
1 1 2	\$	14T 60	0210
2 2 3	\$	14T 60	0220
3 3 4	\$	14T 60	0230
4 4 5	\$	14T 60	0240
5 5 6	\$	14T 60	0250
6 6 7	\$	14T 60	0260
7 7 8	\$	14T 60	0270
CONSTANTS E 432.E3 ALL	\$	14T 60	0280
\$POSSIBLE DEGREES OF FREEDOM INCLUDE TRANSLATION Y ROTATION X Z	\$	14T 60	0290
JOINT RELEASE	\$	14T 60	0300
2 7 MOMENT X Z	\$	14T 60	0310
1 MOMENT Z TH2 -30.	\$	14T 60	0320
MEMBER 1 TO 7 PROPERTIES PRISMATIC IX 38.15 IZ 19.79	\$	14T 60	0330

LOADING 1 'DEAD LOAD'	\$ CROSS SECTIONAL AREA=14.65	\$ 14T 60	0340
MEMBERS 1 TO 7 LOAD	FORCE Y GLOBAL UNIFORM W -2.2	\$ 14T 60	0350
LOADING 2 'OVERTURNING'		\$ 14T 60	0360
MEMBERS 1 TO 7 LOAD	FORCE Y GLOBAL UNIFORM W 0.2	\$ 14T 60	0370
MEMBERS 1 TO 7 LOAD	MOMENT X UNIFORM W -.7	\$ 14T 60	0380
LOADING 3 'LIVE LOAD SPAN 1'		\$ 14T 60	0390
MEMBER 1 LOAD	FORCE Y GLOBAL UNIFORM W -.68	\$ 14T 60	0400
LOADING 4 'LIVE LOAD SPAN 2'		\$ 14T 60	0410
MEMBER 2 TO 6 LOAD	FORCE Y GLOBAL UNIFORM W -.68	\$ 14T 60	0420
LOADING 5 'LIVE LOAD SPAN 3'		\$ 14T 60	0430
MEMBER 7 LOAD	FORCE Y GLOBAL UNIFORM W -.68	\$ 14T 60	0440
LOADING 6 'LIVE LOAD SPAN 1-2'		\$ 14T 60	0450
MEMBER 1 TO 6 LOAD	FORCE Y GLOBAL UNIFORM W -.68	\$ 14T 60	0460
LOADING 7 'LIVE LOAD SPAN 2-3'		\$ 14T 60	0470
MEMBER 2 TO 7 LOAD	FORCE Y GLOBAL UNIFORM W -.68	\$ 14T 60	0480
LOADING 8 'LIVE LOAD SPAN 1-3'		\$ 14T 60	0490
MEMBER 1 7 LOAD	FORCE Y GLOBAL UNIFORM W -.68	\$ 14T 60	0500
LOADING 9 'LIVE LOAD ALL SPANS'		\$ 14T 60	0510
MEMBER 1 TO 7 LOAD	FORCE Y GLOBAL UNIFORM W -.68	\$ 14T 60	0520
PRINT DATA		\$ 14T 60	0600
DUMP TIME		\$ 14T 60	0610
STIFFNESS ANALYSIS		\$ 14T 60	0620
LIST FORCES REACTIONS DISPLACEMENTS		\$ 14T 60	0630
LOAD LIST 3 TO 9		\$ 14T 60	0640
LIST FORCE ENVELOPE MEMBERS 2 TO 6 SECTION FRACT NS 2 0. 1.0		\$ 14T 60	0650
LOAD LIST 1 2		\$ 14T 60	0660
LIST SECTION FORCES MEMBERS 1 7 SECTION FRACT DS 0. .2		\$ 14T 60	0670
LIST SECTION FORCES MEMBERS 2 TO 6 SECTION FRACT NS 2 0. 1.0		\$ 14T 60	0675